

## Overview of Reservoir Simulation and Risk Assessment for WESTCARB's Kimberlina Phase III Pilot



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**WESTCARB Annual Meeting**  
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## Outline

**Part 1**

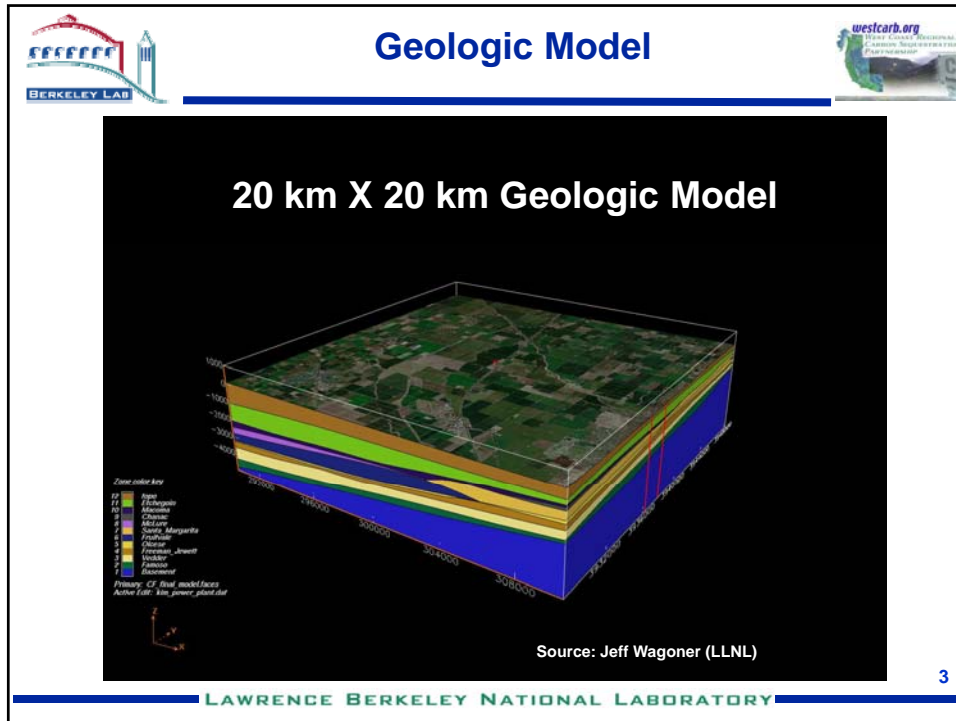
- **Overview of reservoir simulation**
  - Geologic model
  - TOUGH2/ECO2N
  - Results
  - Evolution of mobile fraction

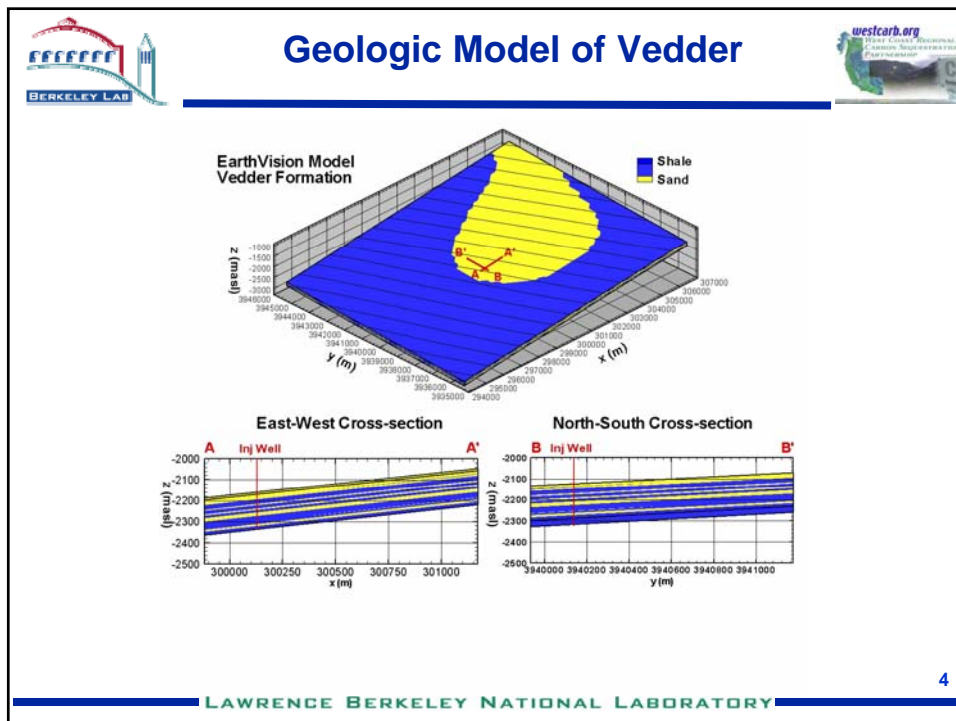
**Part 2**

- **Application of the Certification Framework (CF) to K3**
  - Characterization (surface, hydrology, geology)
  - Reservoir modeling
  - Likelihood of CO<sub>2</sub> and brine intersecting conduits
  - CO<sub>2</sub> and brine leakage risk

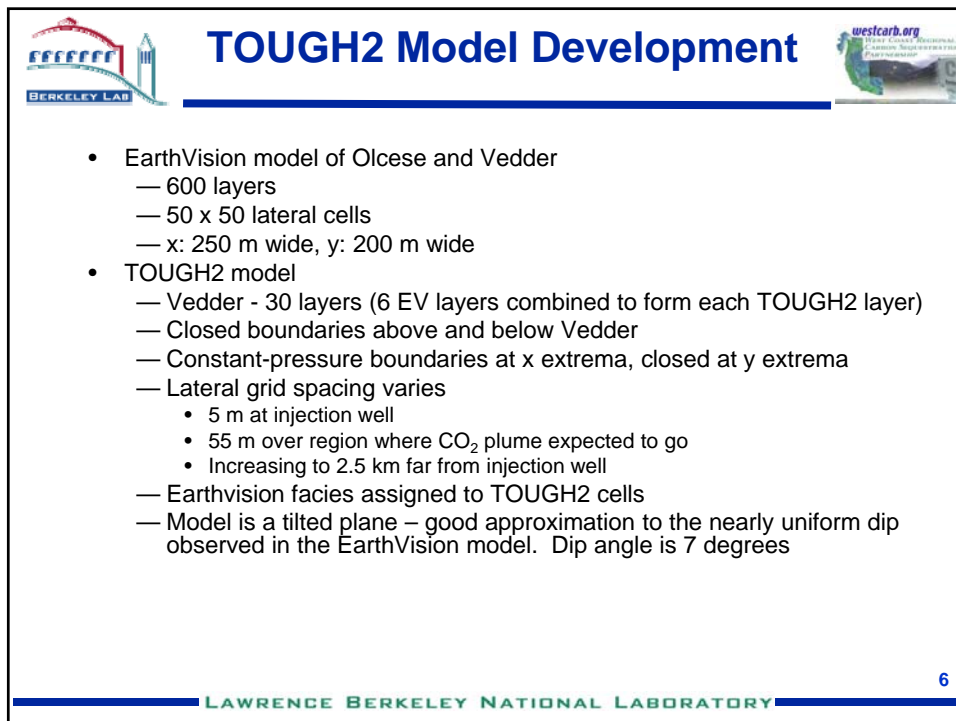
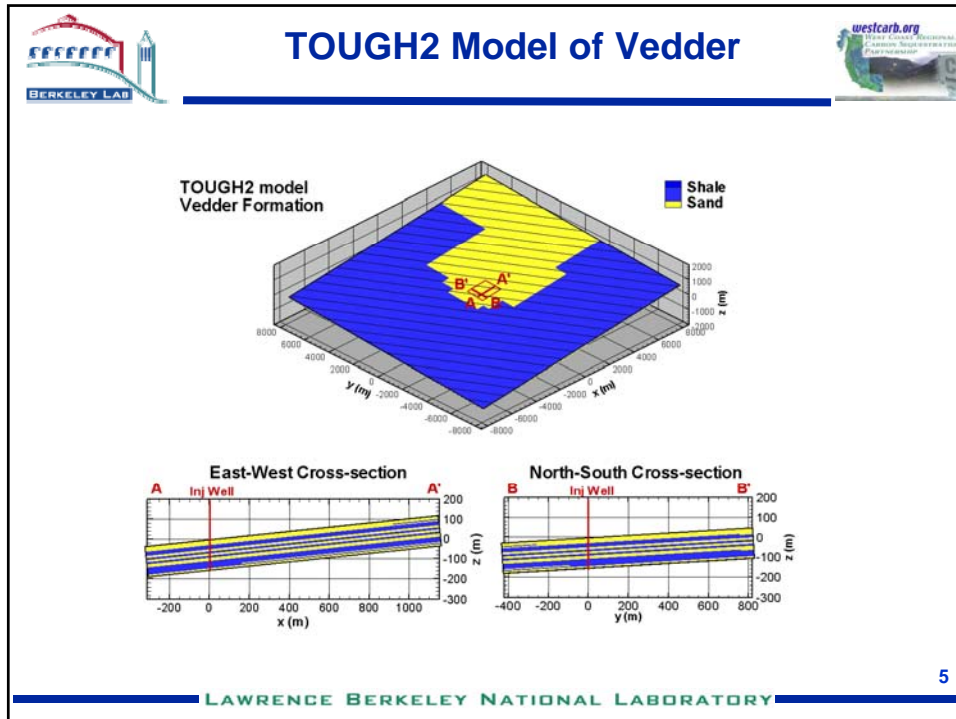
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## Model Parameters




Facies	Porosity	Horizontal Permeability	Vertical Permeability	Residual Liquid Saturation	Maximum Residual Gas Saturation
Sand	28%	200 md	20 md	0.2	0.28
Shale	15%	0.1 md	0.01 md	0.3	0.29


- Residual gas saturation
  - zero during drainage
  - non-zero during imbibition, depends on saturation history

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## CO<sub>2</sub> Injection in Vedder

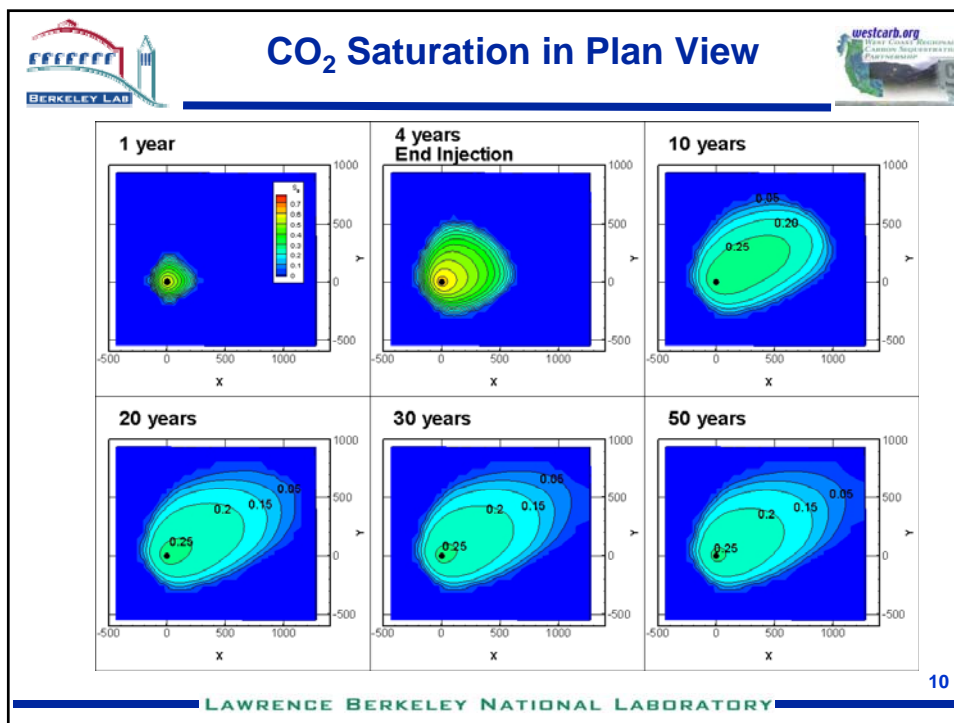
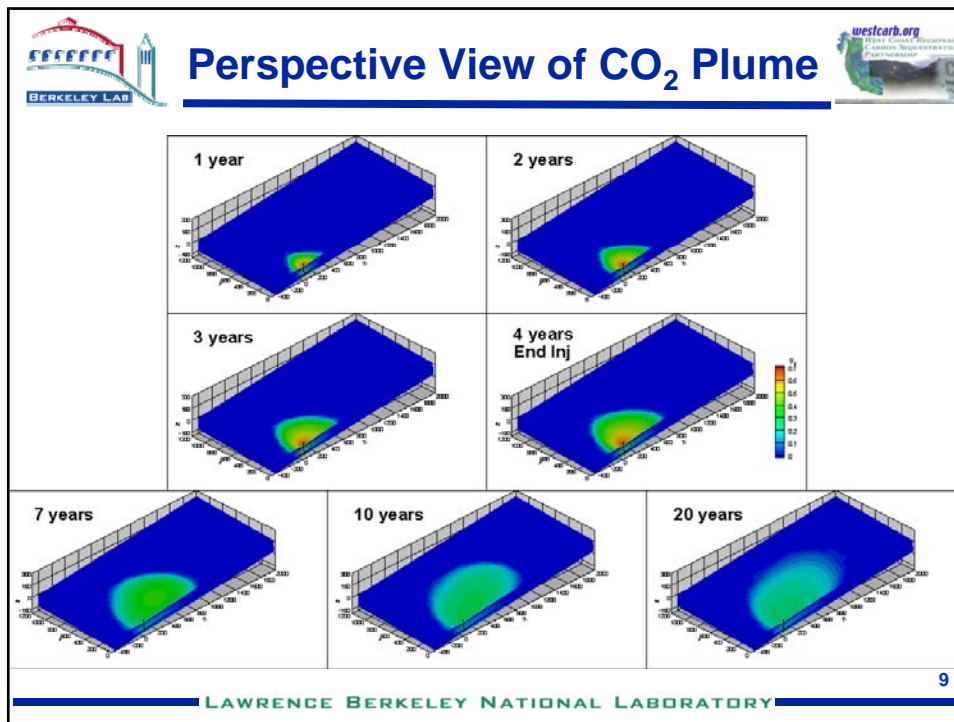


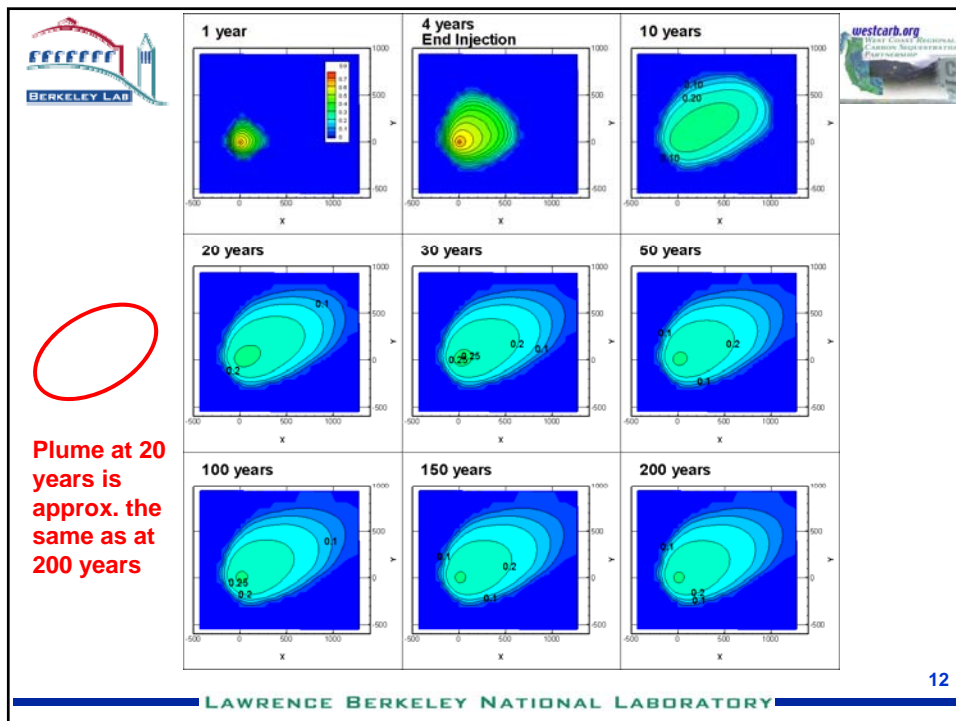
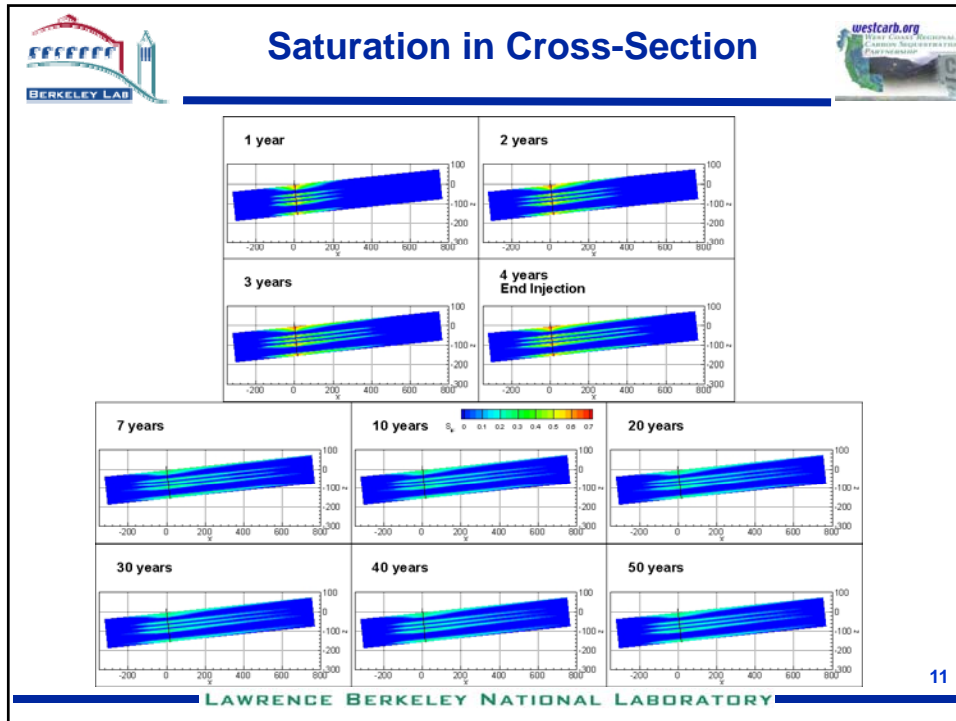
  

- Inject 250,000 t per year for 4 years
- Inject over entire thickness of Vedder (158 m thick)
- At injection location, about 50/50 sand/shale, so net sand thickness is about 79 m
- P = 220 bars, T = 81°C, density of CO<sub>2</sub> = 632 kg/m<sup>3</sup>

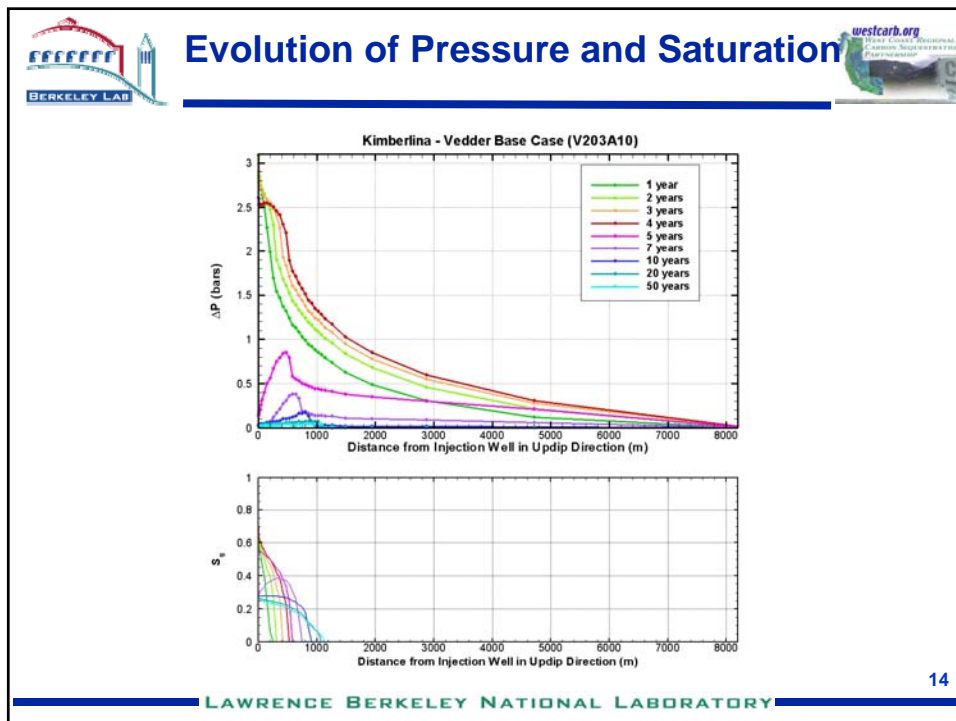
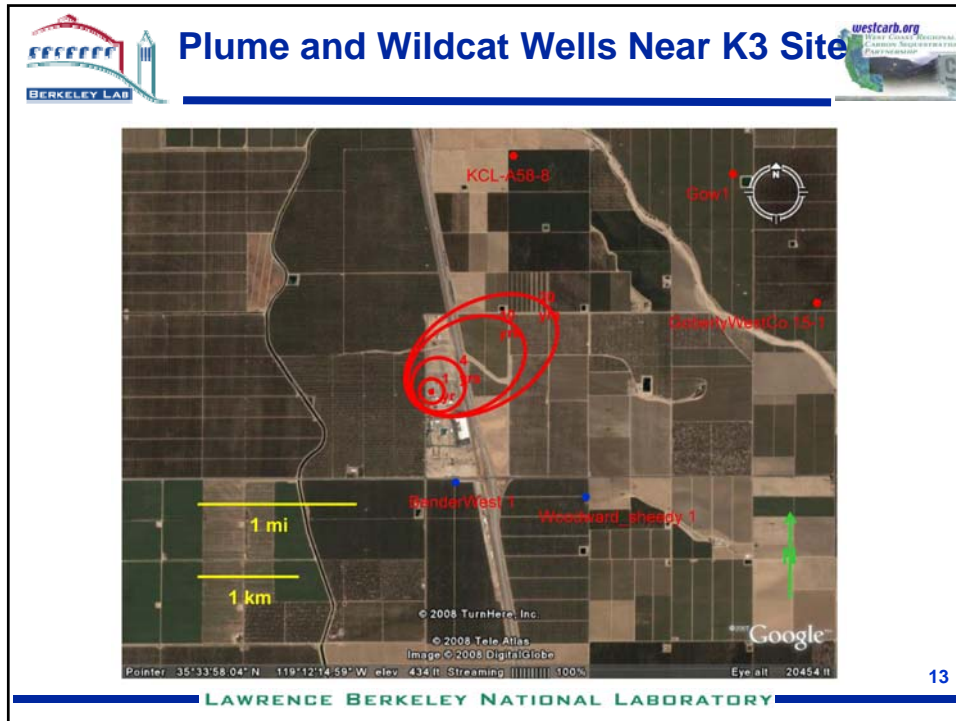
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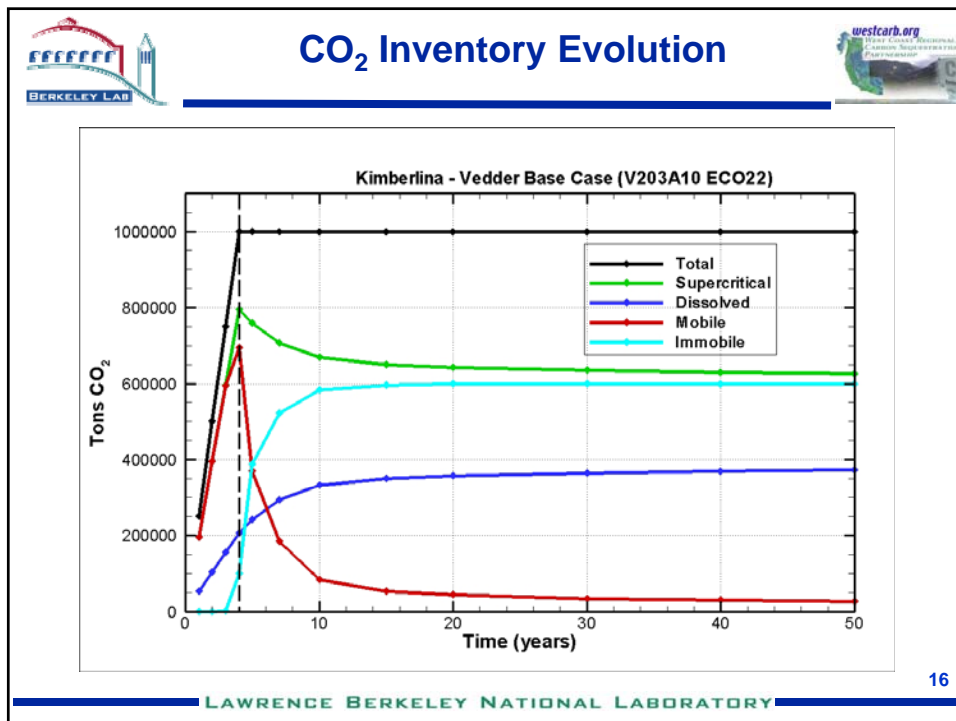
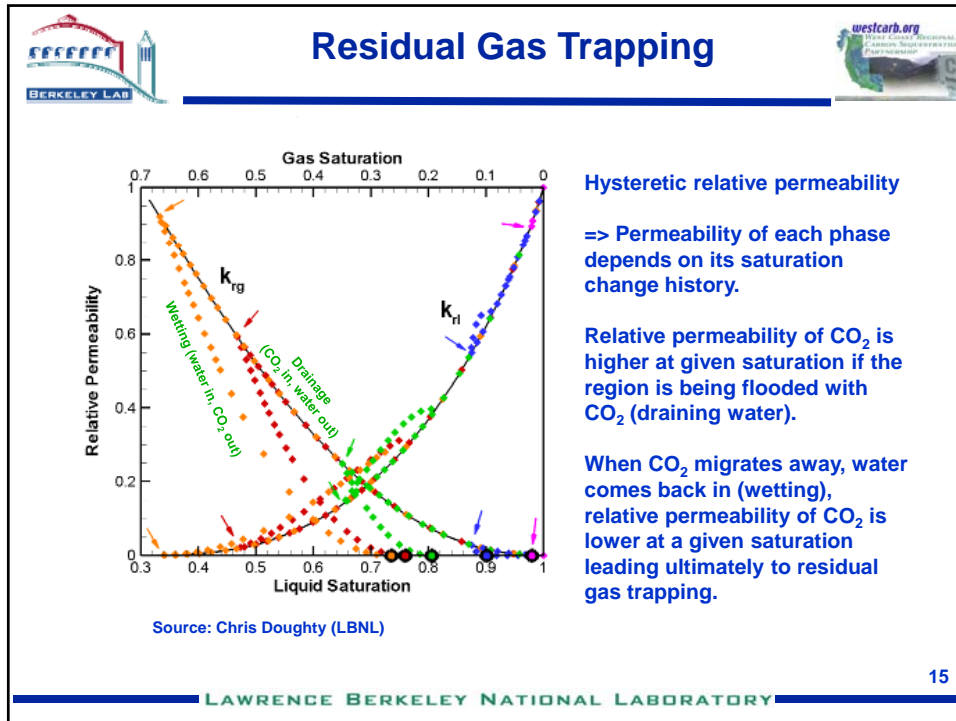





  
**Plume at 20 years is approx. the same as at 200 years**













## Geological Carbon Sequestration Certification Framework




### Part 2: Risk Assessment for WESTCARB's Kimberlina Phase III Pilot

**Curt Oldenburg**  
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LBNL




**Steve Bryant**  
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**Jeff Wagoner**  
LLNL





**Mary Jane Coombs**  
UCOP




**JP Nicot**  
Texas Bureau of  
Economic Geology





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## Kimberlina Phase III Pilot (K3)





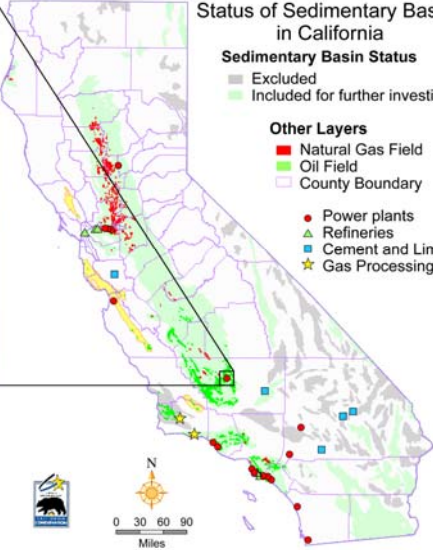
Status of Sedimentary Basins in California

**Sedimentary Basin Status**


- Excluded
- Included for further investigation

**Other Layers**


- Natural Gas Field
- Oil Field
- County Boundary
- Power plants
- ▲ Refineries
- Cement and Lime
- ★ Gas Processing Plants




250,000 t CO<sub>2</sub>/yr for four years


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**K3 Injection in a Nutshell**




- CO<sub>2</sub> sourced from ~50 MW oxy-combustion power plant
- Inject 250,000 t CO<sub>2</sub> per year for 4 years at power plant site
- Inject over entire thickness of Vedder (160 m thick)
- At injection location, about 50/50 sand/shale => net sand thickness is about 80 m
- Top of Vedder is at a depth of 2300 m
- Vedder P = 220 bars, T = 80°C, density of CO<sub>2</sub> = 630 kg/m<sup>3</sup>
- Cap rock is Freeman-Jewett shale (100 m thick)
- Overlying this is the Olcese sand (200 m thick)
- Cap rocks to Olcese are Round Mountain/Fruitvale, McLure, and Macoma (all shale aquitards) totaling 700 m of thickness

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## Preliminary FEP Analysis




- Quintessa online FEP database
  - Features = characteristics such as geometry and flow properties
  - Events = abrupt changes in Features or Processes such as earthquakes
  - Processes = dynamics such as fluid flow or phase change
- 143 FEPs in Quintessa database
- We sorted FEPs into three groups
  - Group 3 = not relevant (78)
  - Group 2 = low probability or low impact or not in scope of K3RA (44)
  - Group 1 = very relevant (21)
- Screening done assuming K3 pilot parameters—not long-term GCS
- All Group 1 FEPs turned out to be either Features or Processes (no Events)

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## Group 1 FEPs




**Table 4-1. Important FEPs treated in this report.**


R	Ca	Cl	FEP#	Category, Class, or FEP Description	Comments
1			2.2.5	Remedial actions	This topic is somewhat out of scope but a good site should have characteristics allowing for quick and effective remedial action. The limited number of deep wells suggests that it is manageable to retrofit them all in the unlikely case of leakage. Similarly, the small amount of CO <sub>2</sub> injected would make it relatively easy to pressurize the Cloose Sand and invert the pressure gradient.
1			3.1.1	Physical properties of CO <sub>2</sub>	Injection depth is known. Temperature and pressure are extrapolated (see FEP# 4.1.13 and 4.1.14). The well-known and defensible code TOUGH2 is used (see Section 5.1)
1			3.1.2	CO <sub>2</sub> phase behavior	See FEP# 3.1.1
1			3.1.3	CO <sub>2</sub> solubility and aqueous speciation	See FEP# 3.1.1
1			3.2.1	Effects of pressurization of reservoir on caprock	Addressed in TOUGH2 modeling (see Section 5.1) - Maximum additional pressure due to injection is 3 bars (Figure 5-6) which is few percent of the local fluid pressure and unlikely to bring it to fracture pressure threshold.
1			3.2.5	Mechanical processes and conditions	fault reactivation, fracture creation unlikely – addressed in Section 5.1
1			3.3.1	Advection of free CO <sub>2</sub>	Addressed by TOUGH2 modeling (Section 5.1)
1			3.3.2	Buoyancy-driven flow	Addressed by TOUGH2 modeling (Section 5.1)
1			3.3.6	CO <sub>2</sub> release processes	CO <sub>2</sub> release processes and impacts at the surface or shallow subsurface are treated in CF (Section 6)
1			4.1.3	Reservoir type	Injecting into a saline aquifer - see TOUGH2 results (Section 5.1)
1			4.1.4	Reservoir geometry	Specific geometric properties have been included into the TOUGH2 model (Section 5.1)
1			4.1.6	Caprock or sealing formation	Described in Section 3.2.1. Primary and secondary seals. Permeability and capillary entry pressure not known
1			4.1.8.2	Pore Architecture	Porosity and permeability are discussed in Section 5.1
1			4.1.10	Heterogeneities	Described in Section 3.2.4
1			4.1.11	Faults and fractures	Described in Section 3.2.3
1			4.1.12	Undetected features	Despite the lack of local data, area has been well studied because of the proximity of oil and gas deposits. Unexpected geologic structures are unlikely to be present. Fault distribution is addressed in Section 3.2.3
1			4.1.16	Petrophysical properties	Described in Section 5.1 (porosity, permeability, relative permeability curves, residual saturations); data extrapolated/interpolated from other wells and from expert knowledge
1			4.2.1	Fluid properties	CO <sub>2</sub> properties are addressed in FEP# 3.1.1 to 3.1.3. Generic brine properties are used in TOUGH2 simulations
1			5.2.4	Orphan wells	See Section 6.3
1			7.1.1	Loss of containment	Addressed in CF and on sections on seals (Section 6)
1			7.2.1	Contamination of groundwater	petrographic characteristics (FeOx, clay, feldspar) of aquifers given in Section 3.2.4. Elevated pressure area may not be sufficient for more saline water to reach overlying aquifers – See Appendix D

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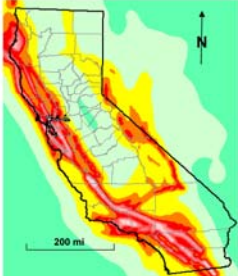


## Some Group 2 FEPs



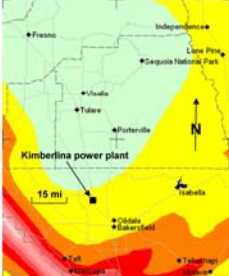
- Seismicity—relatively non-seismic area of CA
- Drilling activities—mostly for water much shallower than Vedder
- CO<sub>2</sub> composition—very pure CO<sub>2</sub> stream from CES plant
- Overpressuring—pressure buildup mostly during 4 years of injection
- Displacement of saline fluids—low-volume injection
- Induced seismicity—injection rate and injectivity compatible with small pressure buildup

(a)




200 mi

(b)




15 mi




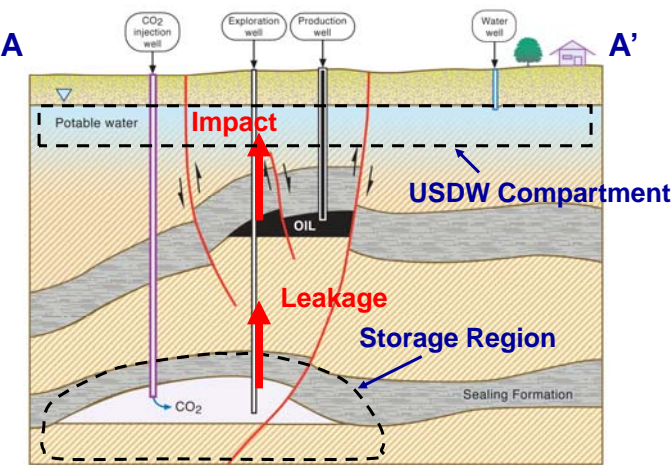
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## CF in a Nutshell



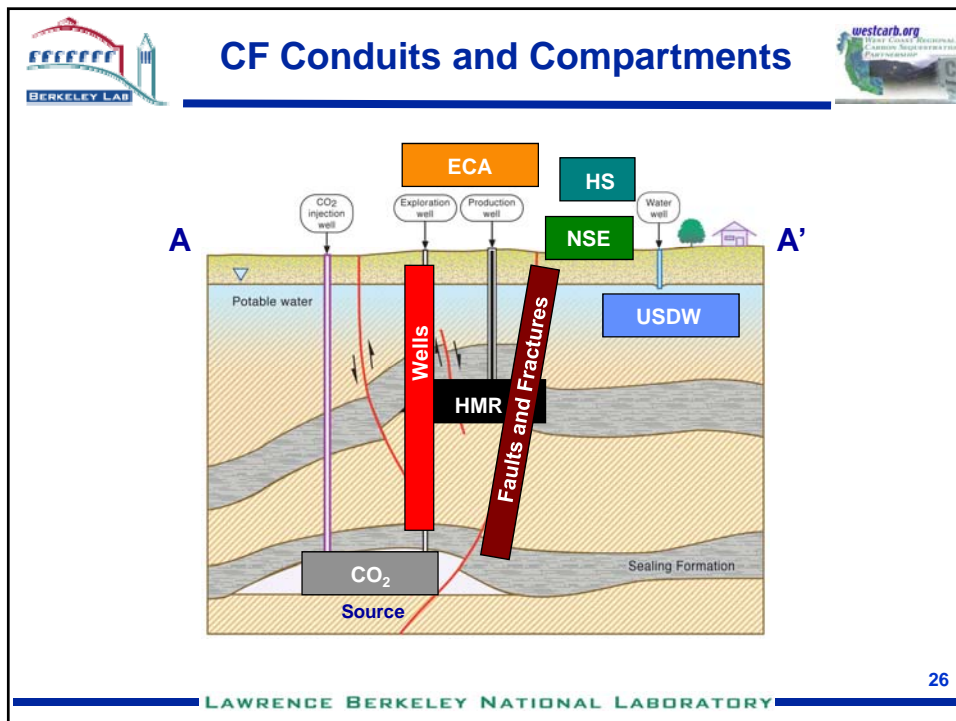
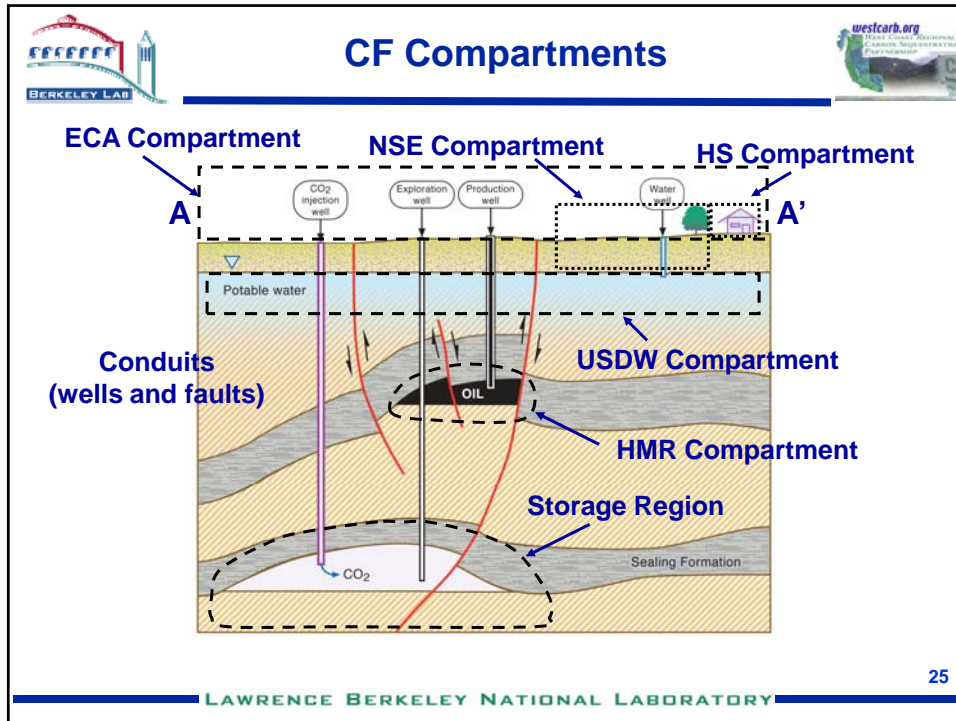


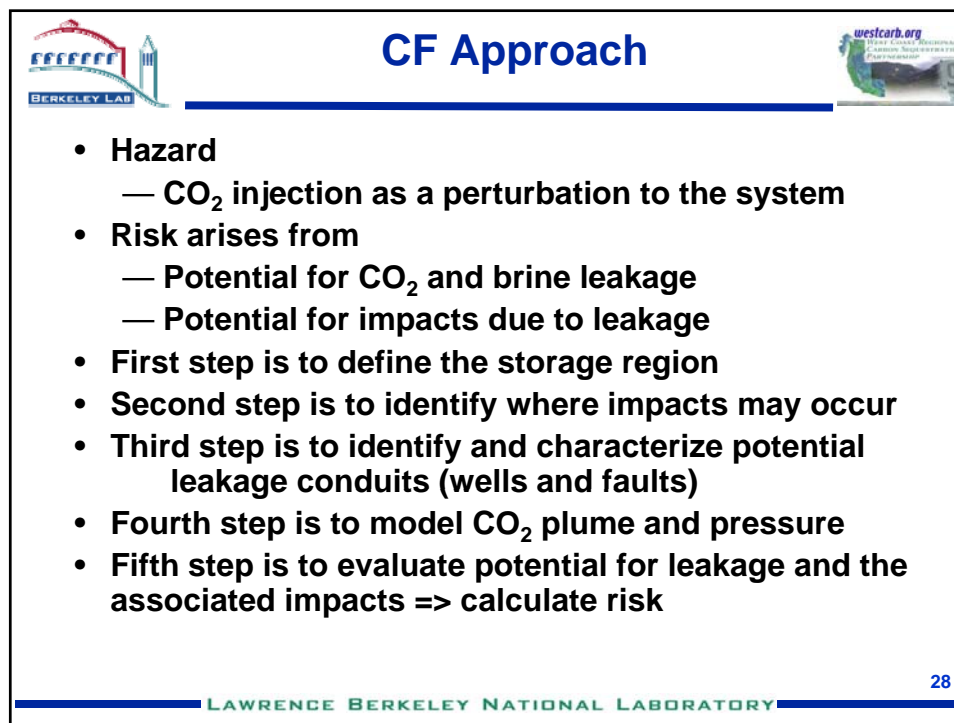
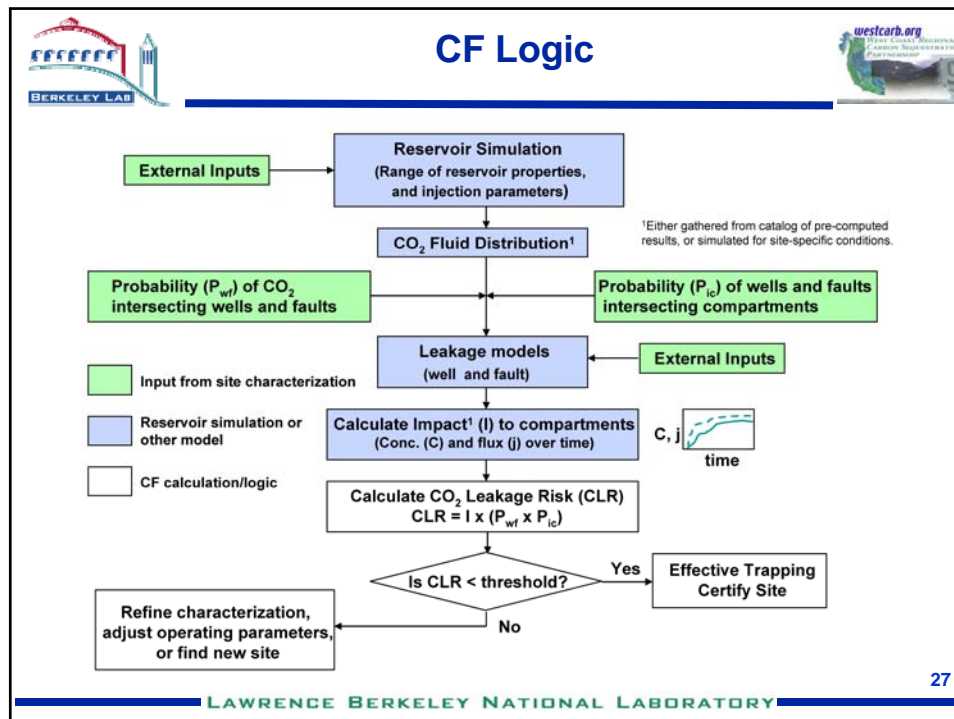



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## 1. Define Storage Region




**First step is to define the storage region**

- Vedder Formation from injection well to 10 km (6 mi) radius


**10 km (6 mi) radius from Kimberlina power plant (red dot)**

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## 2. Define Vulnerable Entities



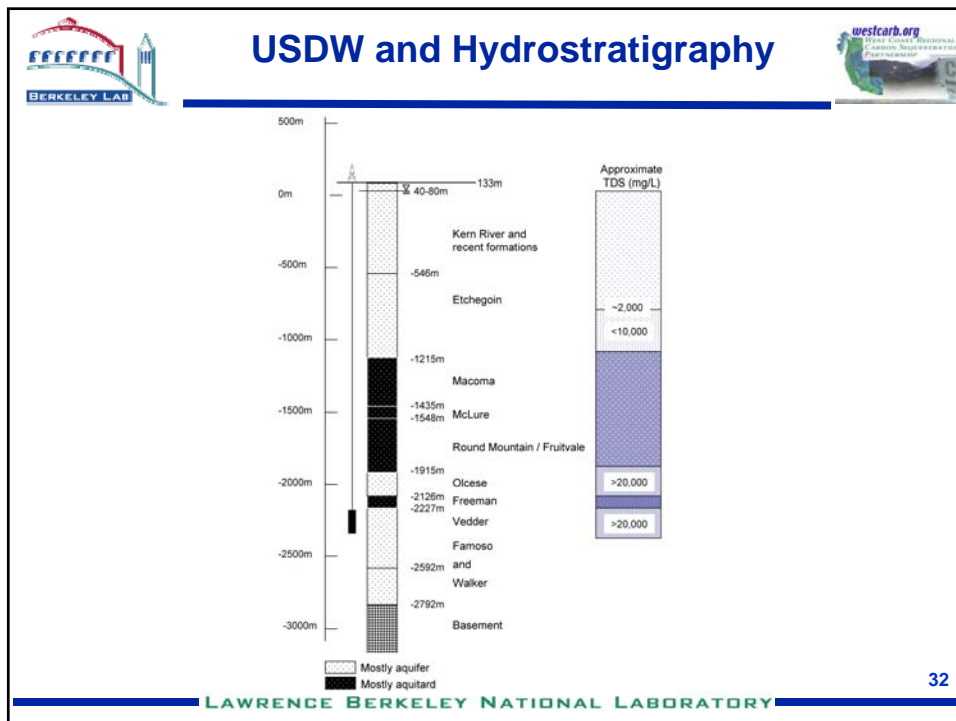
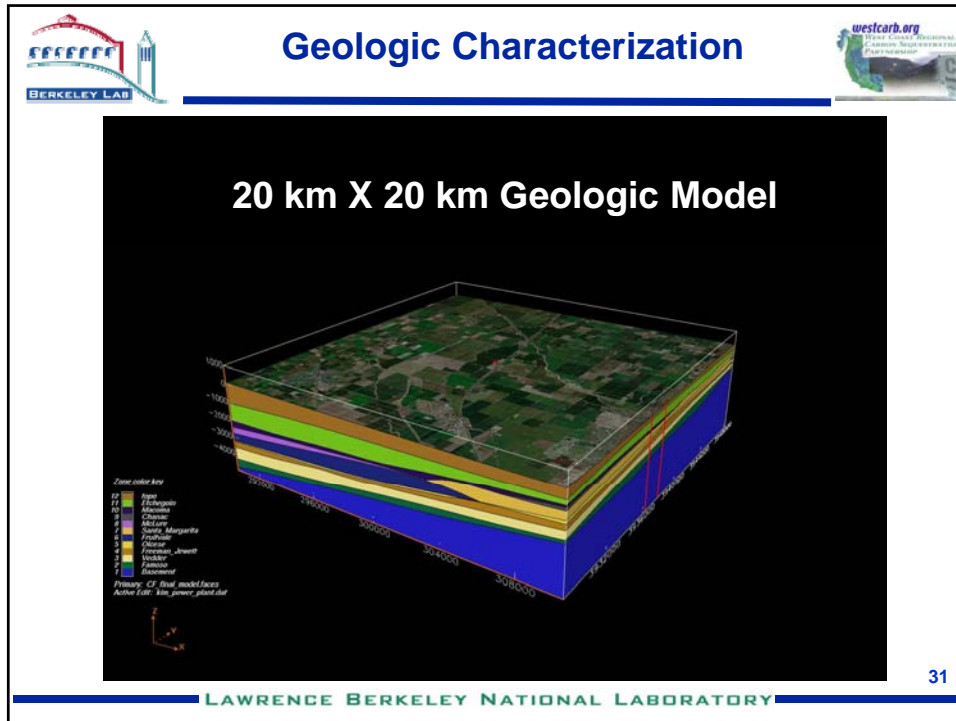
- Topographic relief is minimal.
- Agriculture is primary land use (almond orchards).
- Site is adjacent to U.S. Route 99 and railroad.
- There are a few residences, closest one being 1 km to SW, but generally very sparsely populated.
- Calm conditions, inversion, tule fog in winter.

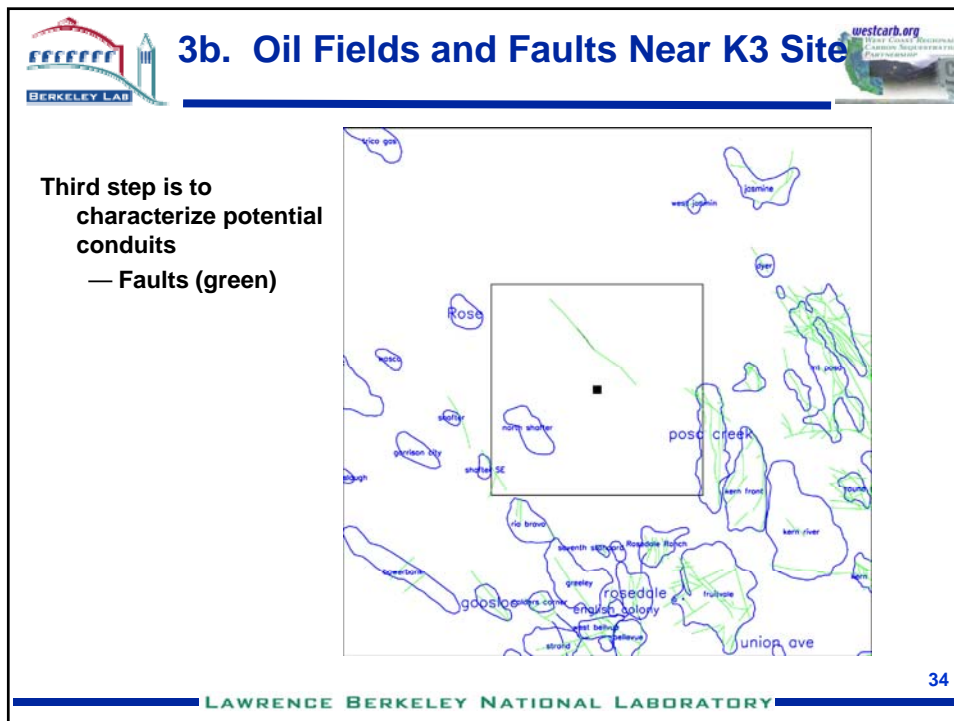
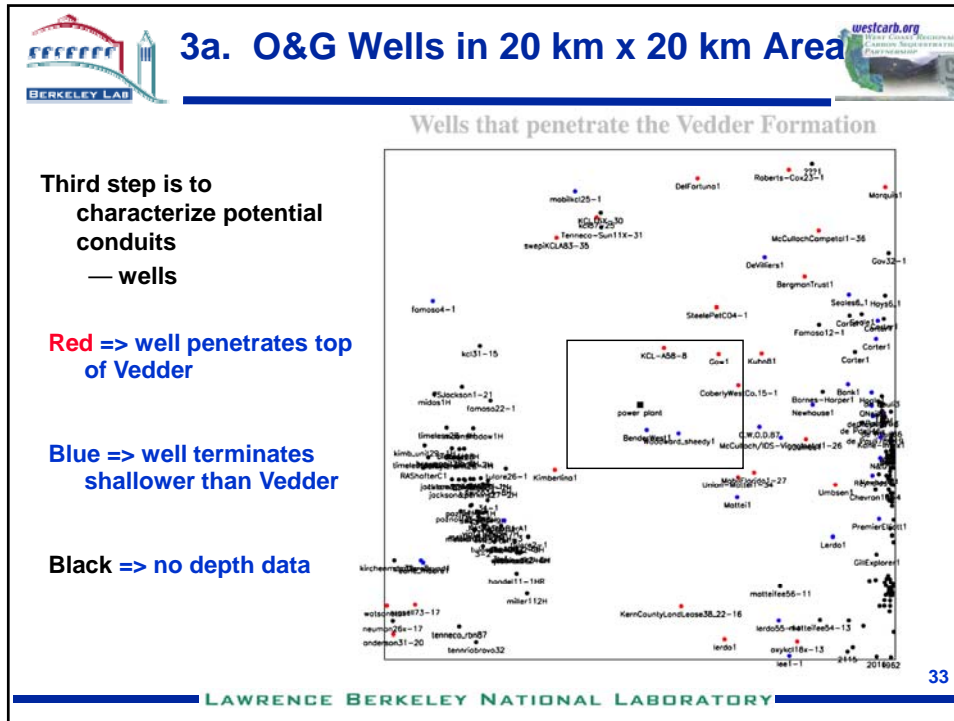
**Bakersfield climate**


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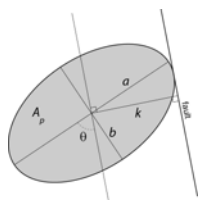




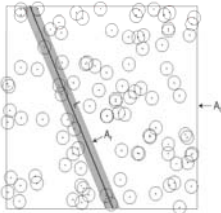
## Faults



- There are no faults mapped at the K3 site
- Fundamentally, some concept of fault density is needed to develop a probability of the plume intersecting a fault.
- Faults occur over a wide range of scales => fault density concept requires specification of size of fault.
- In addition, relation between fault orientation and plume shape is important.
- Lacking site-specific fault data, we measured fault statistical properties determined at surrounding oil fields and assumed the same distributions apply at the K3 site.




(the approach described here was developed by Preston Jordan, LBNL)




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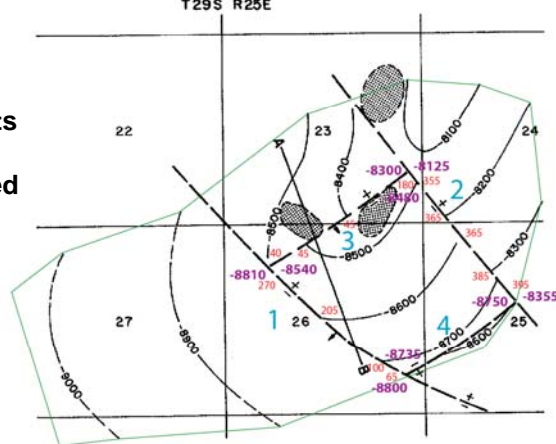


## Example Fault Data



- 956 fault segments were measured

T29S R25E



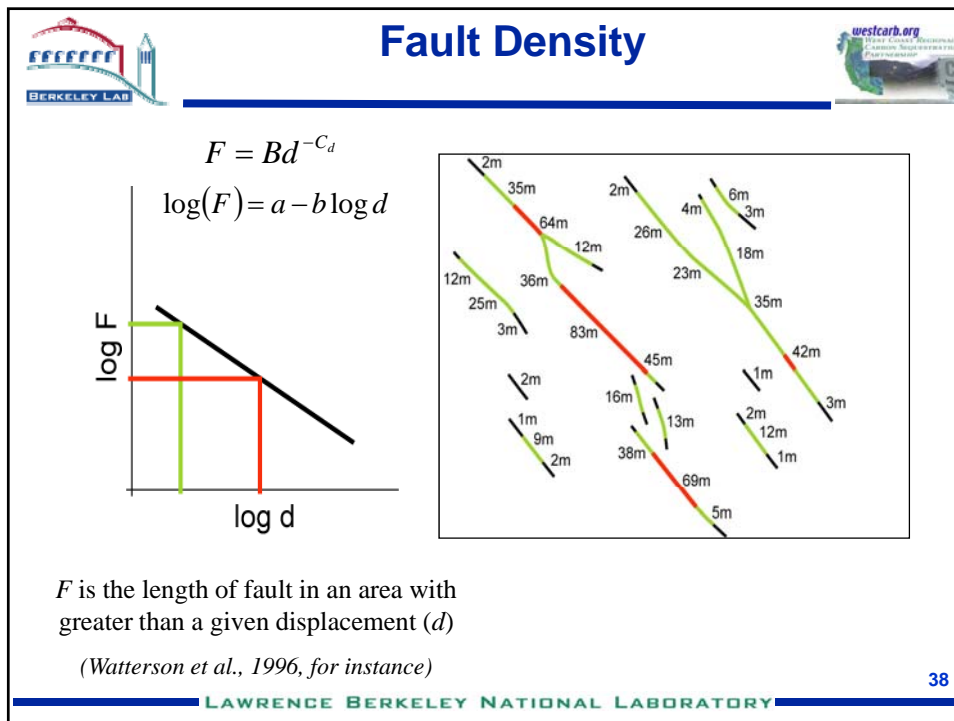
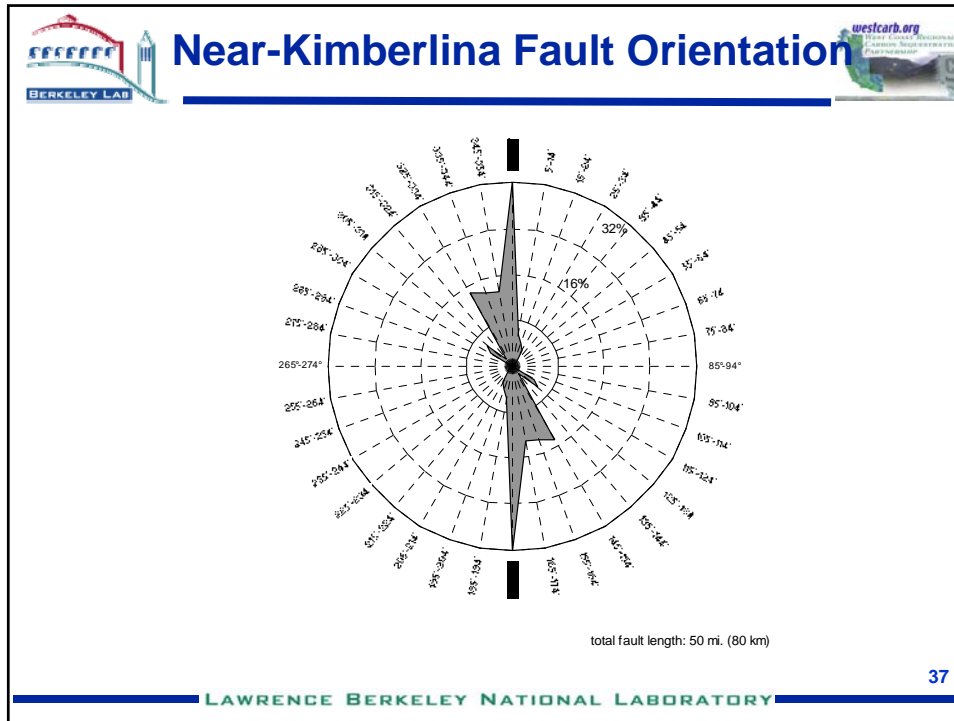
CONTOURS ON TOP OF STEVENS

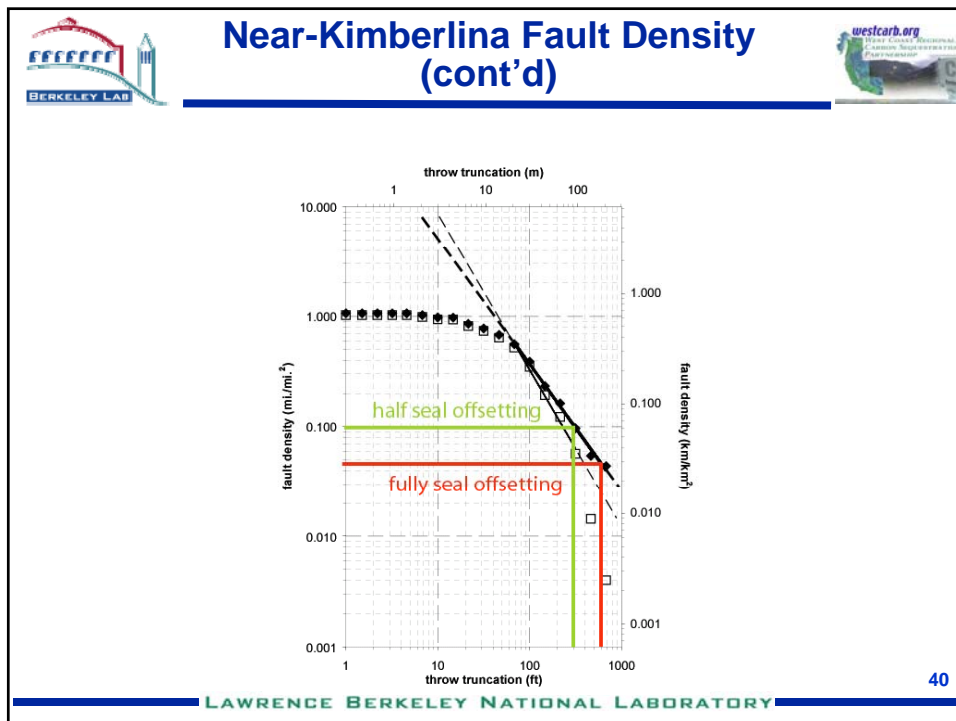
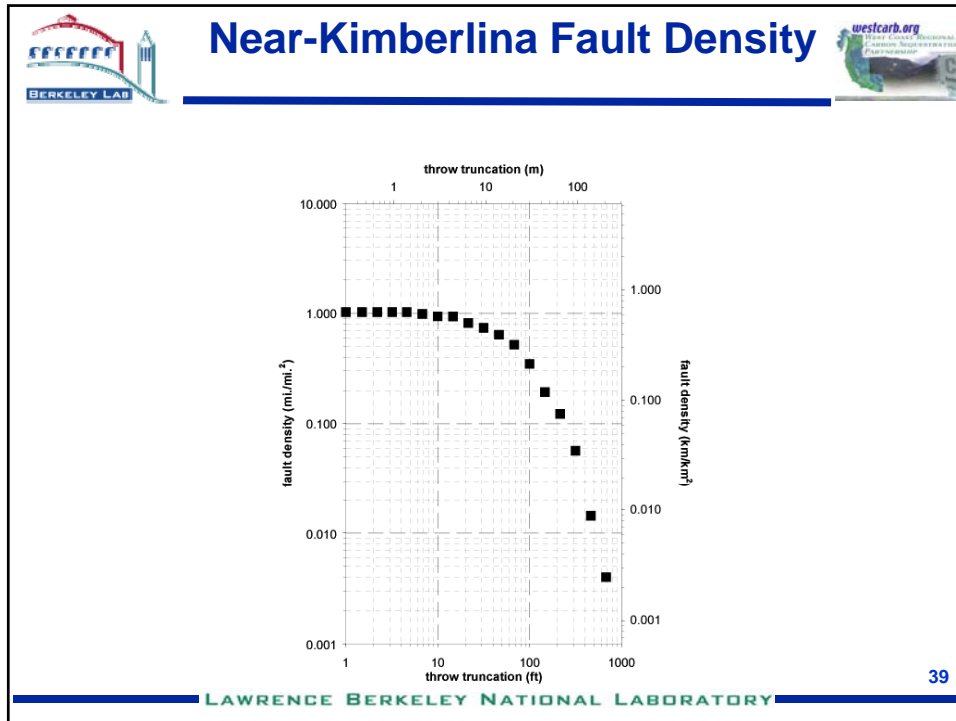
Structure Maps in DOGGR, 1998, CA Oil and Gas Fields, V.1


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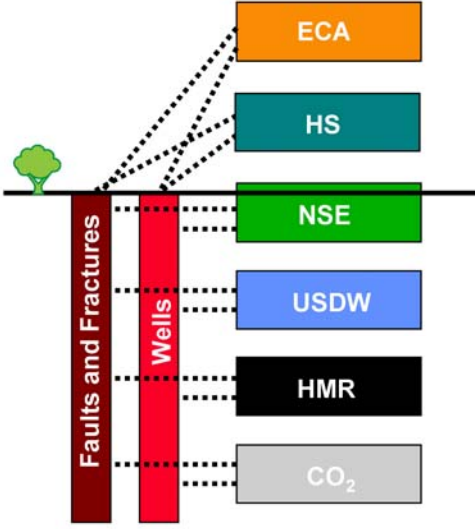






## Potential Intersections







- Emission Credits and Atmosphere
- Health and Safety
- Near-Surface Environment
- Underground Sources of Drinking Water
- Hydrocarbon and Mineral Resources
- CO<sub>2</sub> source


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## 4. Model CO<sub>2</sub> and Pressure







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## 5. Evaluate Leakage Risk




- Sizes of perturbations
  - CO<sub>2</sub> plume
  - Pressure pulse
- Well and Fault intersection probability
  - CO<sub>2</sub> plume
  - Pressure perturbation
- Well and Fault flow potential
  - Permeability
  - Driving force
- Potential for impacts to compartments
- Overall CLR\* and BLR\*\*


\*CLR = CO<sub>2</sub> Leakage Risk  
\*\*BLR = Brine Leakage Risk

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## Sizes of Perturbations

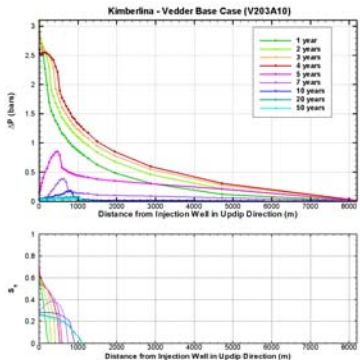


### CO<sub>2</sub> Plume



**Plume is large relative to property lines, small relative to distance to wells and well spacing.**

### Pressure Perturbation




**Pressure pulse is short-lived (<5 years)**


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## CO<sub>2</sub> Plume Conduit Intersection



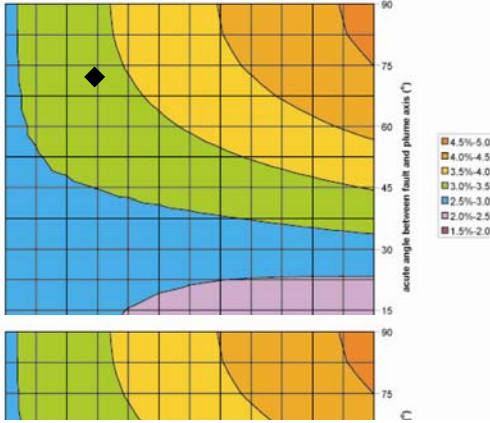
Wells

- Water wells are too shallow to intersect plume.
- Deep wells are sparse.
- CO<sub>2</sub> plume not predicted to intersect deep wells.

Caveats

- Could be unknown wells.
- Plume prediction could be wrong.


Faults




Probability that CO<sub>2</sub> plume will encounter a fault that fully offsets the seal.

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## CO<sub>2</sub> Well and Fault Flow Potential



Wells

- Blowouts 1/15,000 over 20 yrs (Jordan and Benson, 2008).
- Most wells are filled with drilling mud or cement or have cement plugs.

Caveats

- Some wells could be open.

Faults


- Shale-gouge ratio (SGR) suggests seal-offsetting faults will be low-k features.

Caveats


- There are no data on faults at the K3 site.
- There is no oil or gas at the K3 site.
- Fault permeability is notoriously uncertain.

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## Pressure Pulse Intersection




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<p style="text-align: center;"><u>Wells</u></p> <ul style="list-style-type: none"><li>• Multiple wells will be intersected by pressure pulse.</li><li>• Deep wells are sparse.</li></ul>	<p style="text-align: center;"><u>Faults</u></p> <ul style="list-style-type: none"><li>• Multiple faults will be intersected by pressure pulse.</li></ul>
<p style="text-align: center;"><u>Caveats</u></p> <ul style="list-style-type: none"><li>• Could be unknown wells.</li><li>• Pressure prediction could be wrong.</li></ul>	<p style="text-align: center;"><u>Caveats</u></p> <ul style="list-style-type: none"><li>• Could be unknown faults.</li><li>• Pressure prediction could be wrong.</li></ul>


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## Brine Well and Fault Flow Potential




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<p style="text-align: center;"><u>Wells</u></p> <ul style="list-style-type: none"><li>• Blowouts 1/15,000 over 20 yrs (Jordan and Benson, 2008).</li><li>• Most wells are filled with drilling mud or cement or have cement plugs.</li><li>• Elevated pressure does not necessarily lead to significant upflow.<ul style="list-style-type: none"><li>— Low k</li><li>— Density stratified system</li></ul></li></ul>	<p style="text-align: center;"><u>Faults</u></p> <ul style="list-style-type: none"><li>• Elevated pressure does not necessarily lead to significant upflow.<ul style="list-style-type: none"><li>— Low k by SGR</li><li>— Density stratified system</li></ul></li></ul>
<p style="text-align: center;"><u>Caveats</u></p> <ul style="list-style-type: none"><li>• Well properties are uncertain.</li></ul>	<p style="text-align: center;"><u>Caveats</u></p> <ul style="list-style-type: none"><li>• Fault permeability is notoriously uncertain.</li></ul>


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## Impacts



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- **The impacts of potential leakage will be relatively small in this sparsely populated region (e.g., CO<sub>2</sub> discharging at the ground surface).**
- **Emphasis on likelihood of occurrence of low-impact events arises because it is hard to justify expending large resources on modeling low-probability, low-impact events.**
- **Conservative likelihood estimates are consistent with the sparse subsurface data available for the site.**


Table 6-1. Expectation terminology (modified from Hnottavange-Telleen, Schlumberger Carbon Services)

Occurrence expectation terminology	If there were 100 projects like the K3 pilot,
Improbable	...less than once in the 100 projects
Unlikely	...in 1 to 5 of the 100 projects
Somewhat likely	...in 6 to 10 of the 100 projects
Likely	...in 11 to 50 of the 100 projects
Very likely	... more than 50 times within the 100 projects


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## Summary



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- **We have used the CF approach (along with FEP analysis) to analyze CO<sub>2</sub> and brine leakage risk at the K3 site.**
- **We made use of 3D geologic model, and inventory of wells and associated data near the site.**
- **Lack of data on faulting inspired a novel approach to calculating the probability of encountering faults in a statistical sense.**
- **Numerical simulations with TOUGH2 and CMG-GEM provide defensible predictions of CO<sub>2</sub> plume migration.**
- **Based on these data, simulations, and analyses we find the leakage risk for the K3 pilot project to be de minimis.**
- **Additional data gathering, validation of the novel approaches used here, and modeling should be undertaken as the pilot project proceeds.**


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## Acknowledgments



**This work was supported by the CO<sub>2</sub> Capture Project (CCP) of the Joint Industry Program (JIP), by WESTCARB through the Assistant Secretary for Fossil Energy, Office of Sequestration, Hydrogen, and Clean Coal Fuels, National Energy Technology Laboratory (NETL), and by Lawrence Berkeley National Laboratory under Department of Energy Contract No. DE-AC02-05CH11231.**



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